

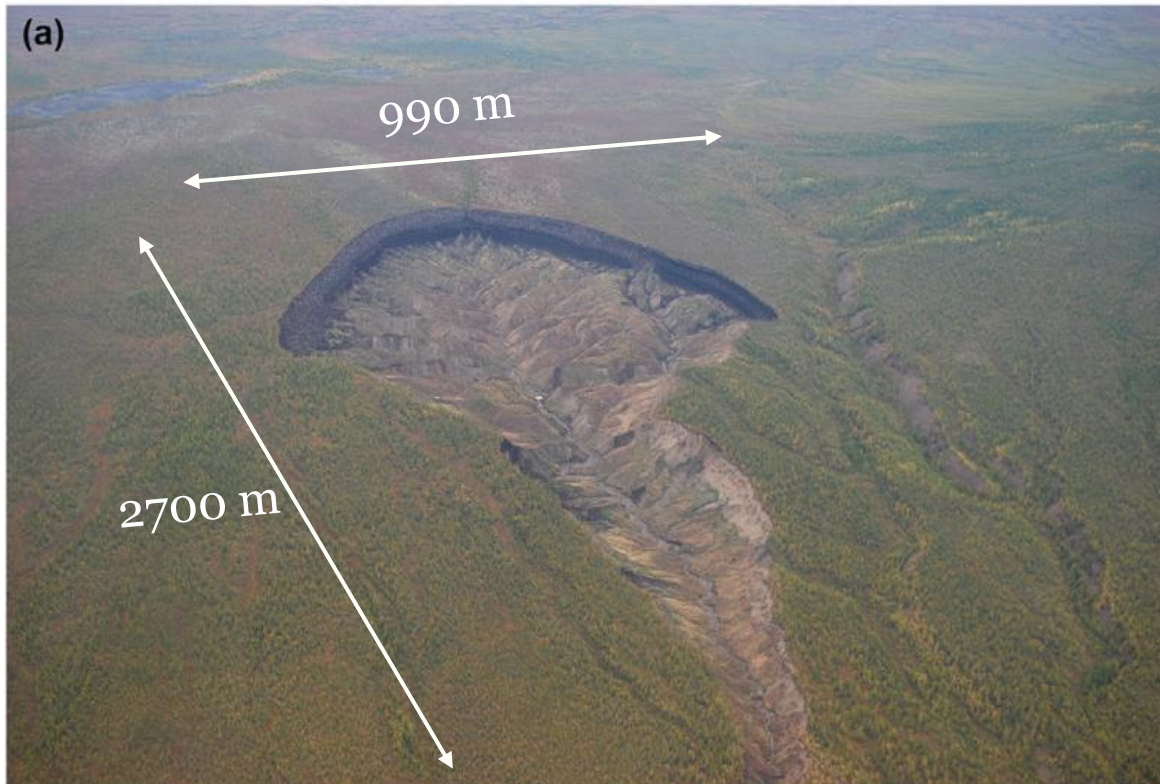
# Effective properties of evolving porous media: From microstructure to macroscopic scale

**Maria OLARTE-GARZON**, Jean-Michel PEREIRA, Patrick DANGLA

# A variety of “frozen” geomaterials

Complex behavior, complex microstructure,  
high heterogeneity

*Example: Batagaika megaslump*

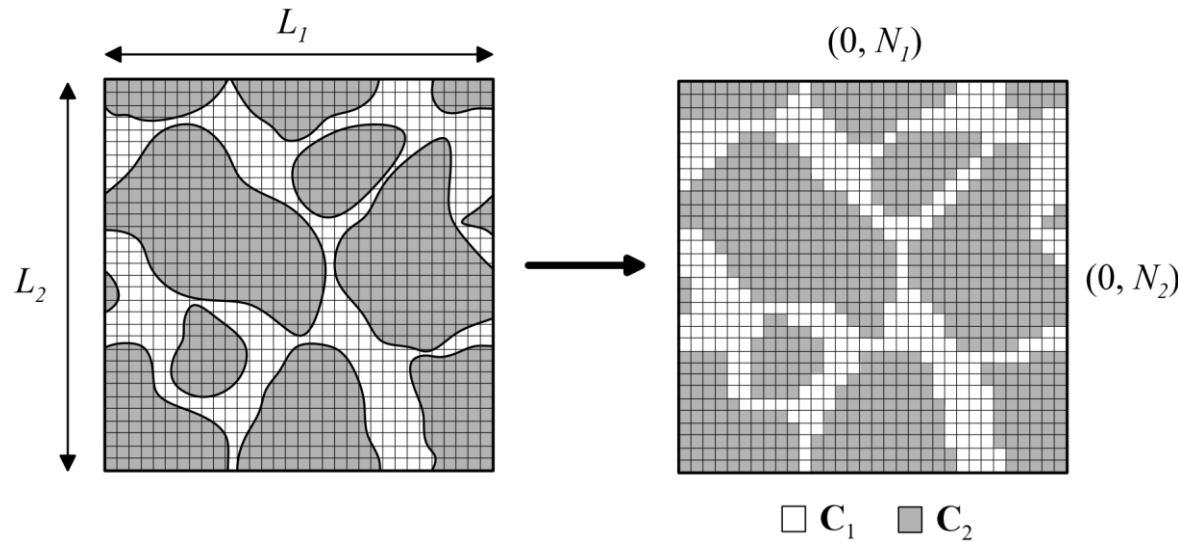
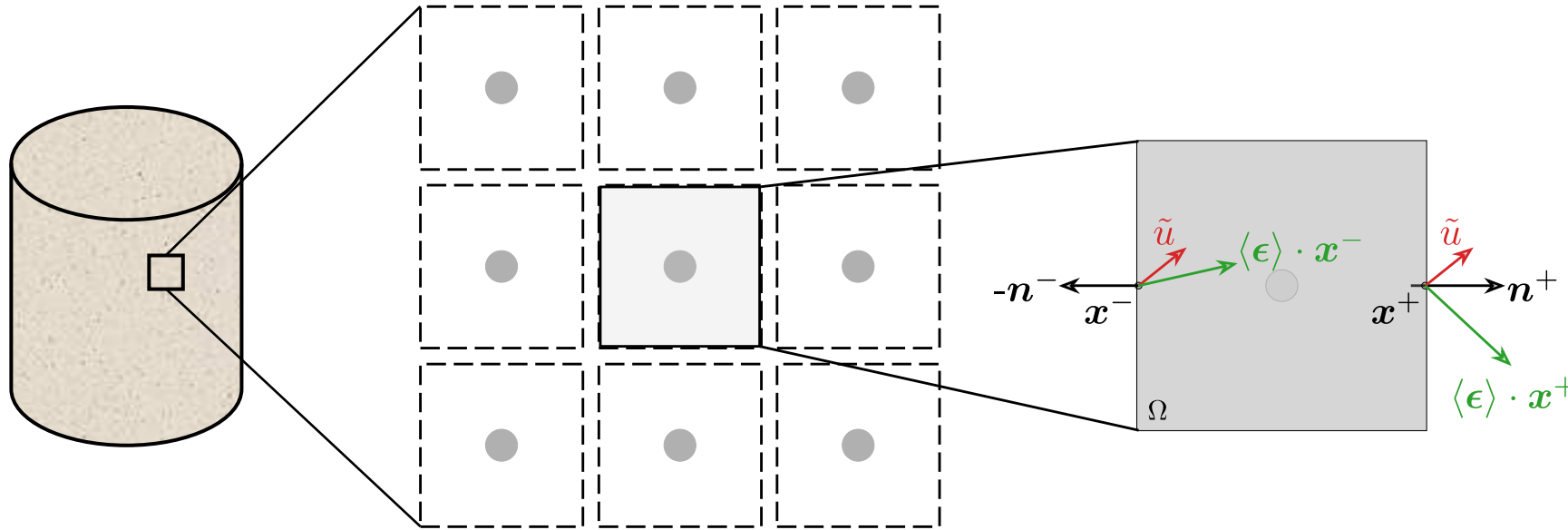


Frozen soils and permafrost in cold regions (ground at or below  $0^{\circ}\text{C}$  for  $\geq 2$  consecutive years) provides a key role for foundation stability for infrastructure (roads, pipelines, buildings).



Murton, J., Opel, T., Wetterich, S., Ashastina, K., Savvinov, G., Danilov, P., & Boeskorov, V. (2023). Batagay megaslump: A review of the permafrost deposits, *Quaternary environmental history, and recent development. Permafrost and Periglacial Processes*, 34(3), 399-416.

# What is periodic homogenization?



## FFT-based homogenisation:

Resolution of a Lippman-Schwinger equation (Moulinec & Suquet, 1994)

Issues with infinite contrasts, treated following Sab et al. (2024)

# Thermoporomechanical couplings

Constitutive relations of the porous solid (Coussy, 2011):

Mechanical	$\underline{\underline{\Sigma}} =$	$\underline{\underline{C}}^{hom} : \underline{\underline{E}}$	$-\underline{\underline{B}}^{hom} P$	$-\underline{\underline{C}}^{hom} : \underline{\underline{A}}^{hom} T$
Hydraulic	$\Phi - \phi_0 =$	$\underline{\underline{B}}^{hom} : \underline{\underline{E}}$	$+\frac{1}{N^{hom}} P$	$-3A_{\phi}^{hom} T$
	$\underline{W} =$		$-\frac{\rho}{\eta} \underline{\underline{K}}^{hom} \cdot \underline{\nabla} P$	
Thermal	$S_s =$	$\underline{\underline{C}}^{hom} : \underline{\underline{A}}^{hom} : \underline{\underline{E}}$	$-3A_{\phi}^{hom} P$	$+H^{hom} T$
	$\underline{Q} =$			$-\underline{\underline{\Lambda}}^{hom} \cdot \underline{\nabla} T$
		Mechanical	Hydraulic	Thermal

$\underline{\underline{E}}$ : Macroscopic strain

$P$ : Macroscopic pore pressure

$T$ : Macroscopic temperature

$\underline{\underline{\Sigma}}$ : Macroscopic stress

$\Phi$ : Macroscopic porosity

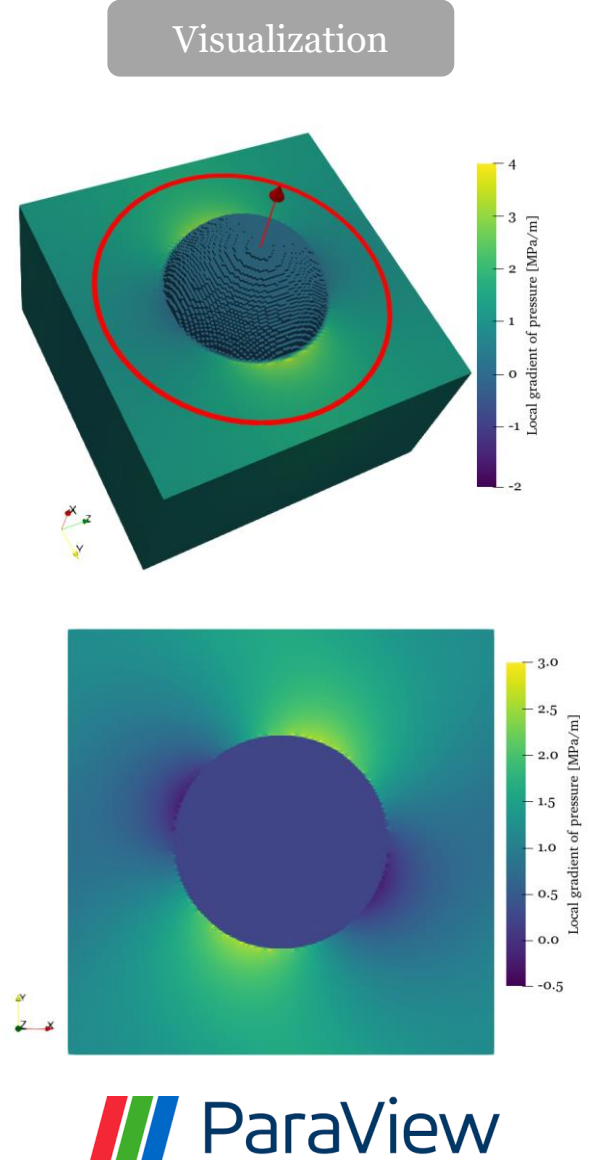
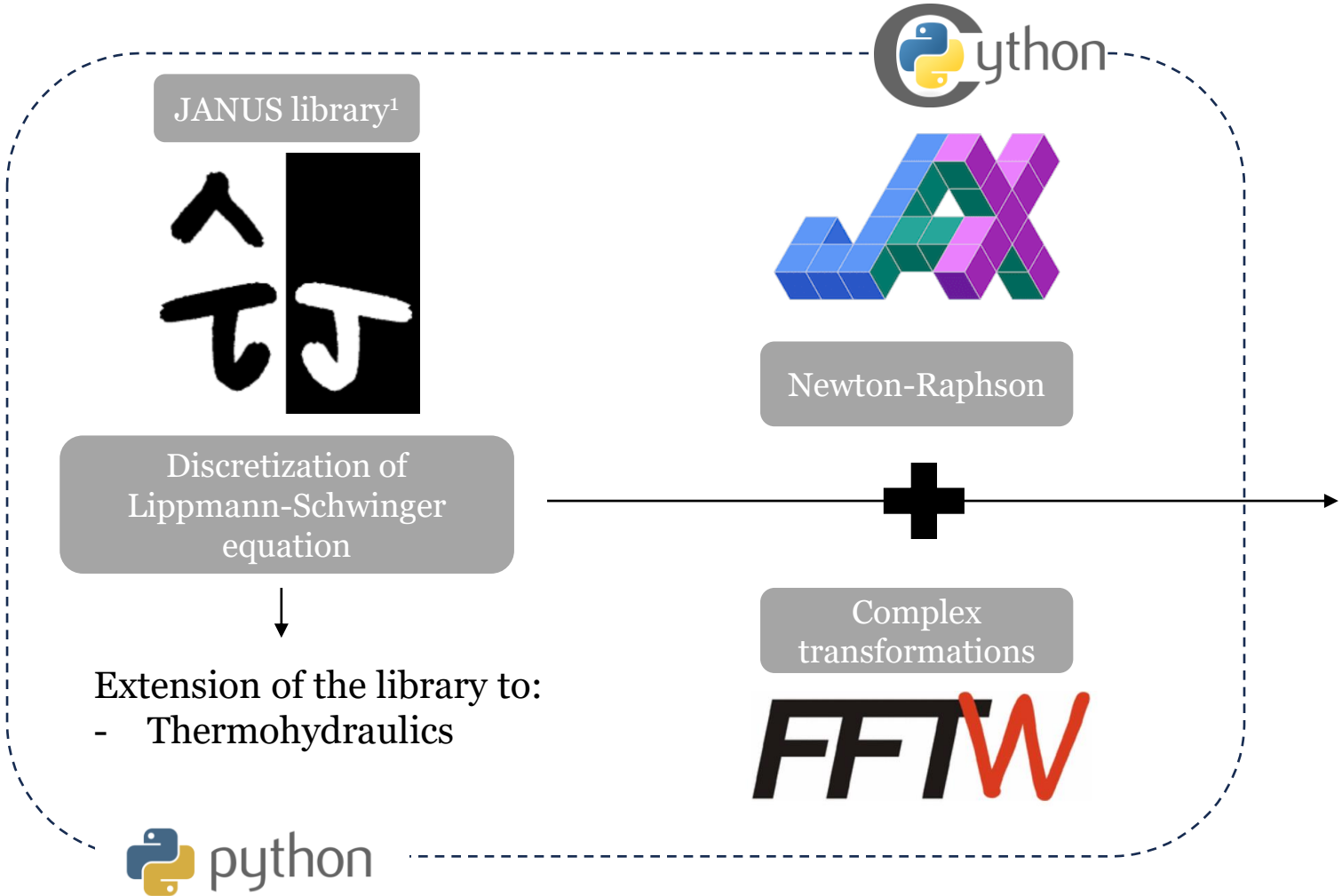
$S_s$ : Macroscopic solid

skeleton's entropy

$\underline{W}$ : Macroscopic flux vector

$\underline{Q}$ : Macroscopic heat vector

# Numerical tool



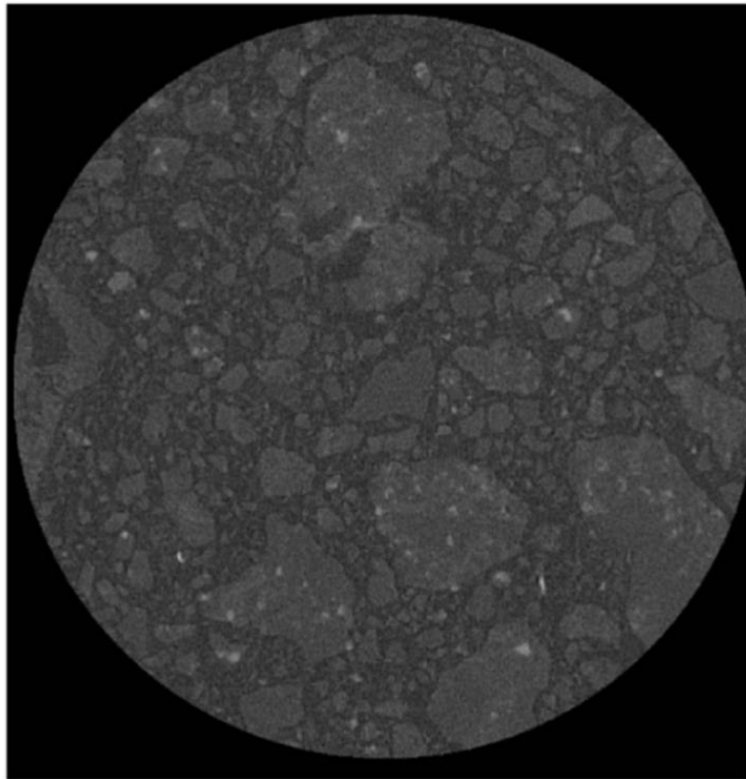
 ParaView

<sup>1</sup> Sébastien Brisard

**Application:  
Nucleation and sublimation in lunar soils**

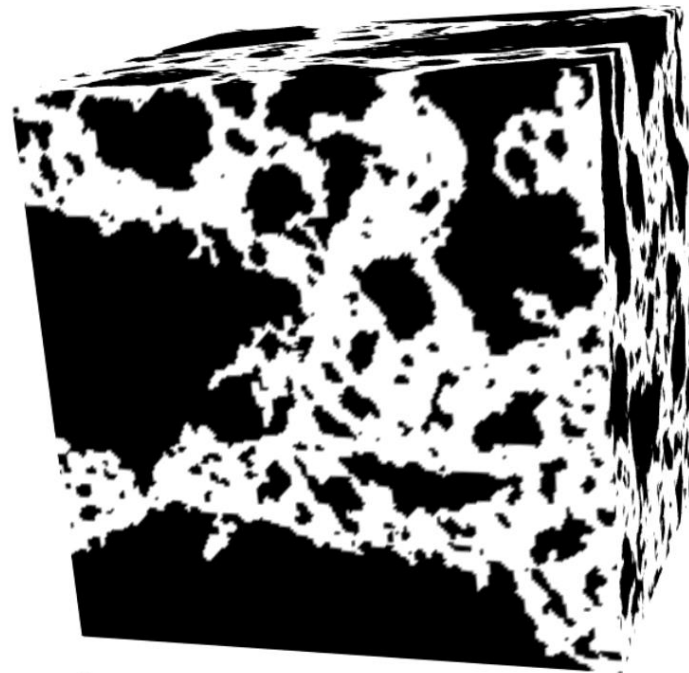
# LUNAR REGOLITH SIMULANT

**Real image**



← 1000 pixel = 1.11 mm →

**Discretized image**



← 200 pixel = 0.222 mm →

## **Simulant properties:**

The simulant consists of plagioclase, pyroxene, ilmenite, and glass.

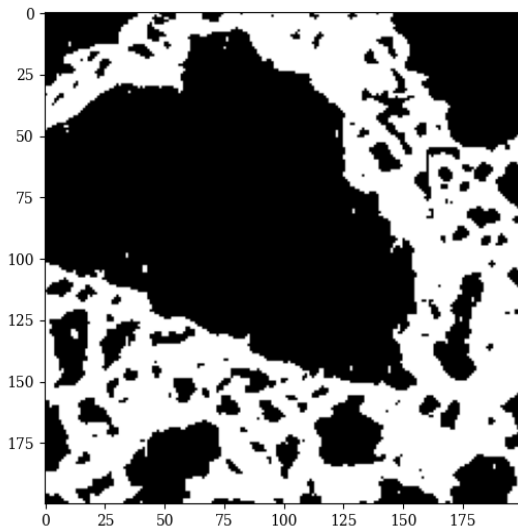
Pixel size of 1.11  $\mu\text{m}$

The complete digital consists of  $1000 \times 1000 \times 1000$  voxels.

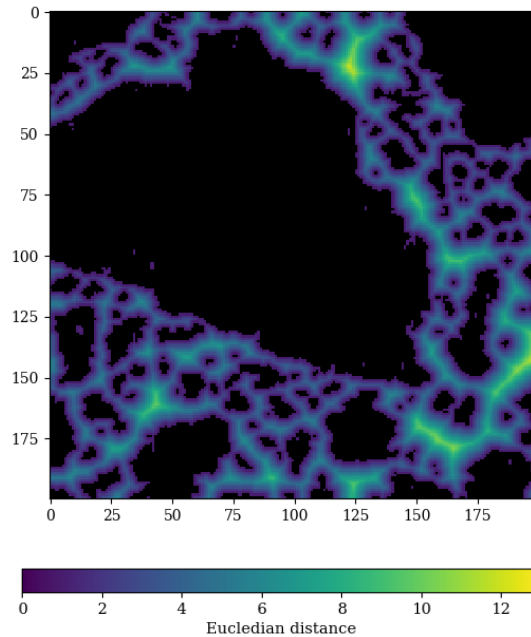
# Soil Freezing Characteristic Curve (SFCC)

## Pore-morphology-based estimation

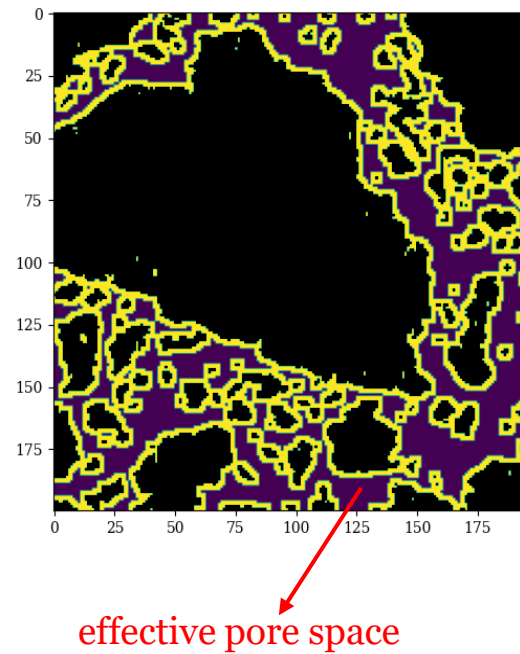
*Binary image*



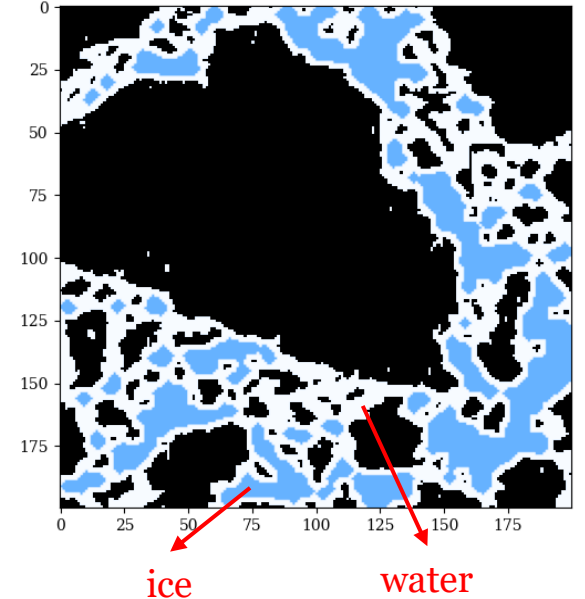
*Distance map*



*Eroded image*



*Openend image*



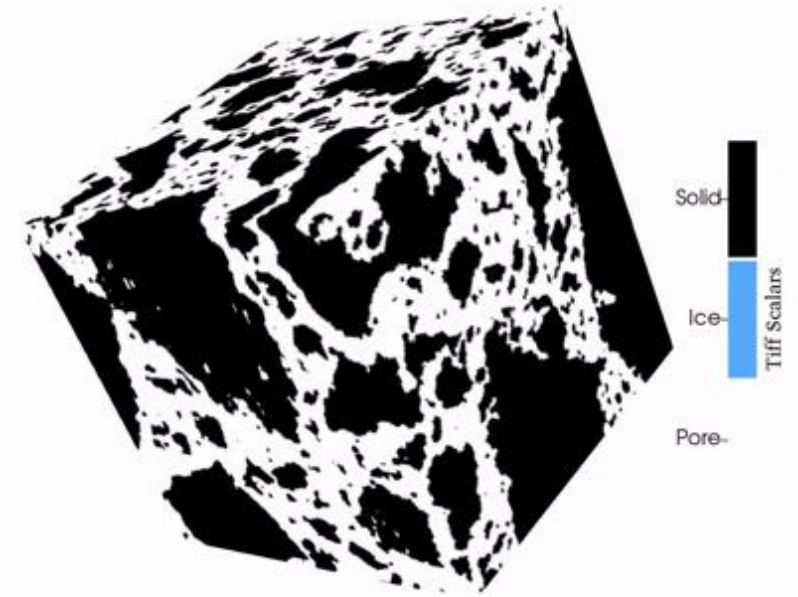
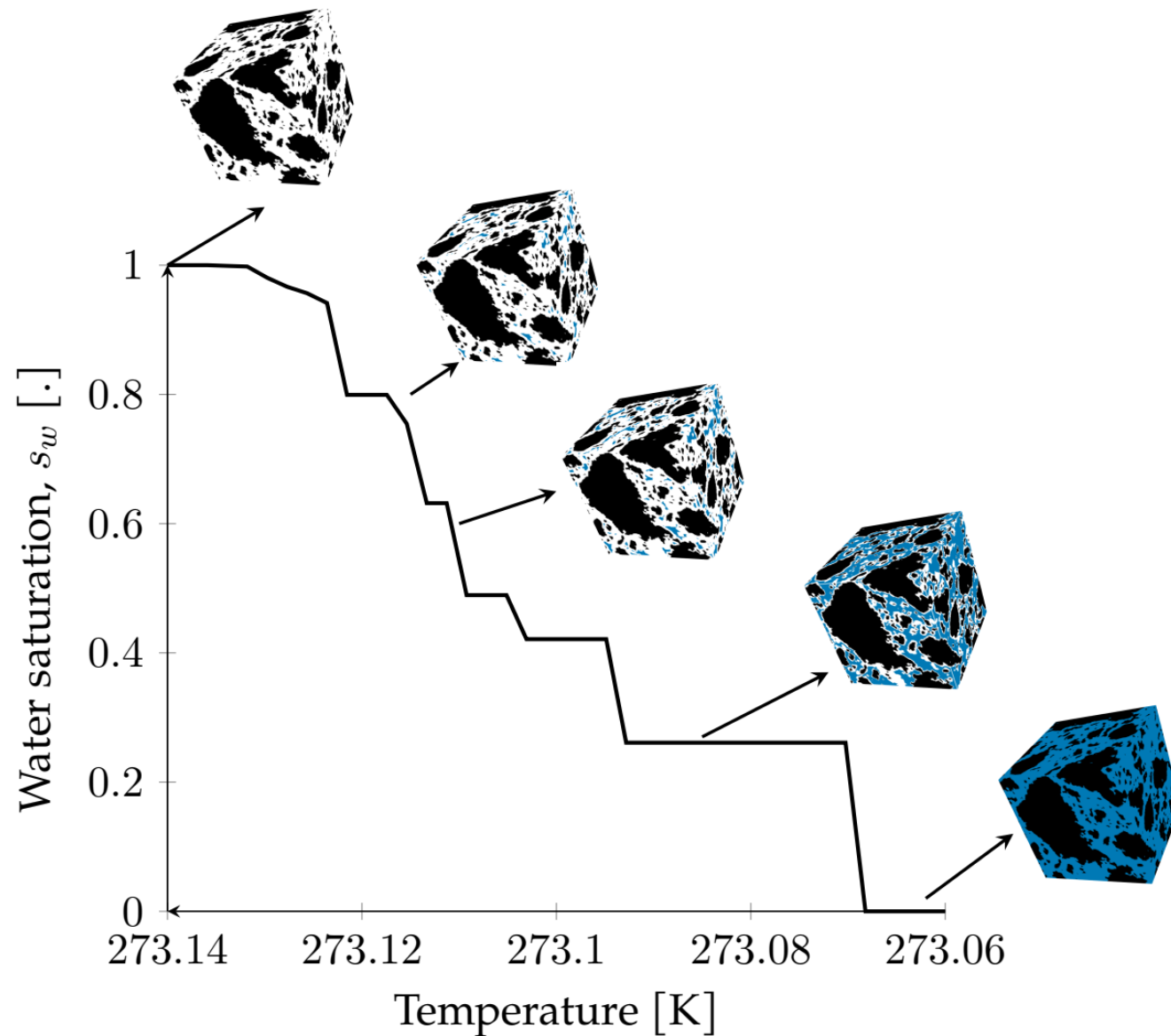
$$d(\hat{\mathbf{x}}_p) = \min_{\hat{\mathbf{x}}_s \in X_s} \|\hat{\mathbf{x}}_p - \hat{\mathbf{x}}_s\|_2$$

$$X_p^{eff} = \{\hat{\mathbf{x}}_p | d(\hat{\mathbf{x}}_p) \geq \hat{r}_p(T)\}$$

Gibbs-Thompson equation:

$$\hat{r}_p(T) = \frac{3\sigma_{iw} \cos \theta}{\rho_i L_f} \left(1 - \frac{T}{T_f^\infty}\right)^{-1}$$

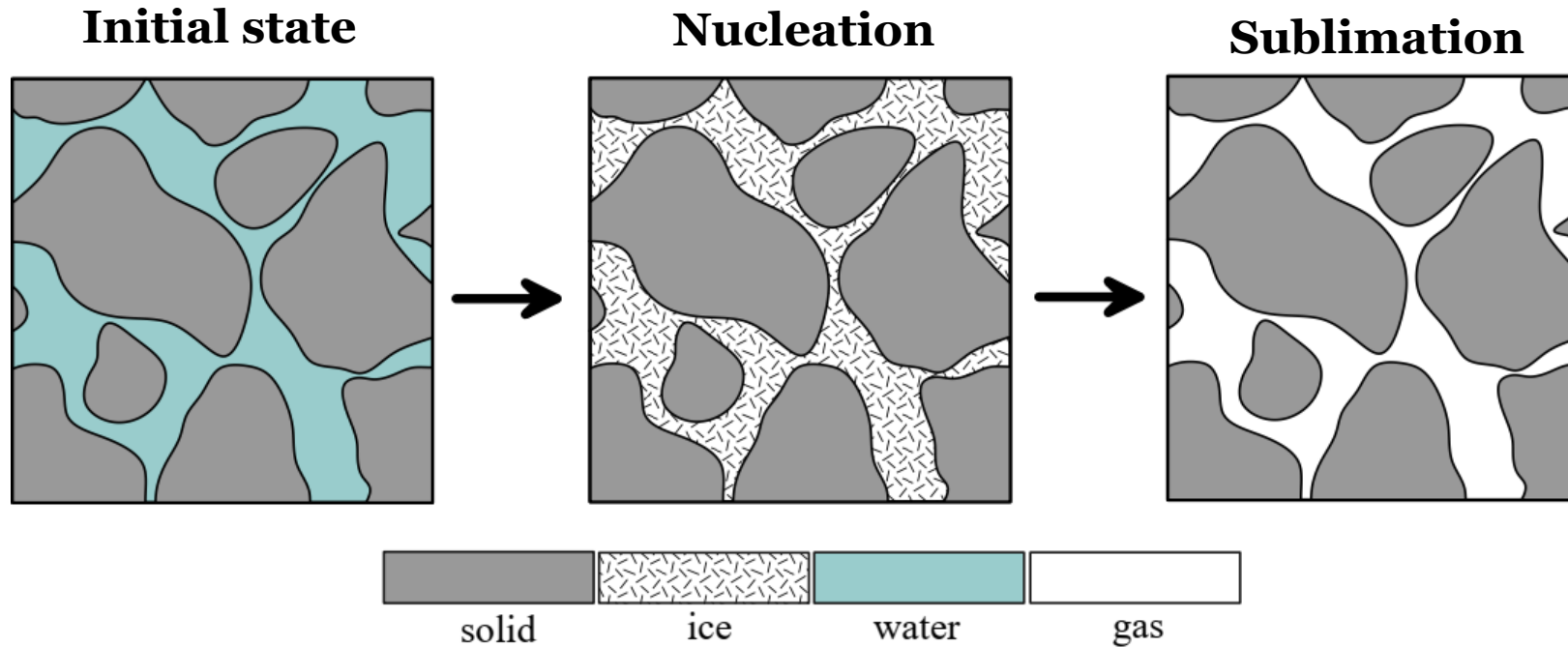
# Soil Freezing Characteristic Curve (SFCC)



Temperature varies from 273.14 K to 273.06 K, and  $s_w$  was recorded at 40 intervals of 0.002 K.

The ice density was kept constant at  $\rho_c = 910 \text{ kg/m}^3$ .

# ELASTICITY



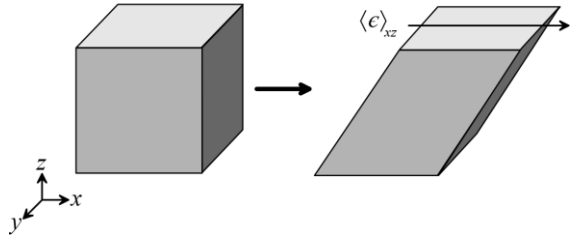
Input parameters of the phases for the FFT-based simulations.

Phase	Mechanics			Transport			
	k [GPa]	g [GPa]	$\nu$ [-]	$d_{CO_2}$ [ $m^2/s$ ]	$\lambda$ [W/(m·K)]	$\mu$ [Pa · s]	$\nu$ [-]
Solid	7.97	4.89	0.24	0.0	0.001* [123], 0.1 [121]	$\infty$	0.5
Water	2.2	0.0	0.5	$1.6 \cdot 10^{-9}$ [124]	0.6 [125]	$1 \cdot 10^{-3}$	0.5
Ice	9.2	3.3	0.33	0.0	2.2 [125]	$\infty$	0.5
Gas	0.0	0.0	0.0	$1.6 \cdot 10^{-5}$ [107]	0.0	-	-

Note: \* corresponds to the value under lunar vacuum conditions.

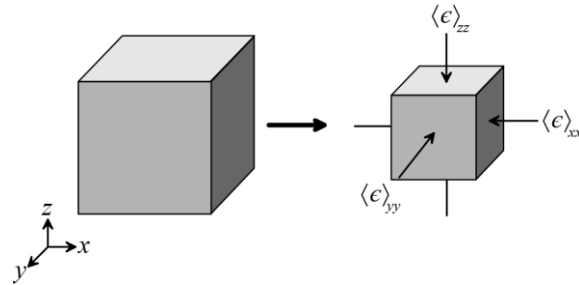
# Loading cases and boundary conditions

## Shearing



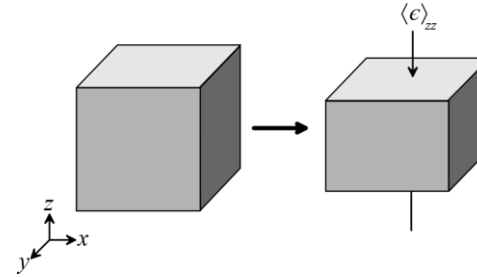
$$d\langle \sigma \rangle_{xz} = G \times 2 d\langle \epsilon \rangle_{xz}$$

## Isotropic



$$d\langle \sigma \rangle_v = K \times d\langle \epsilon \rangle_v$$

## Oedometric

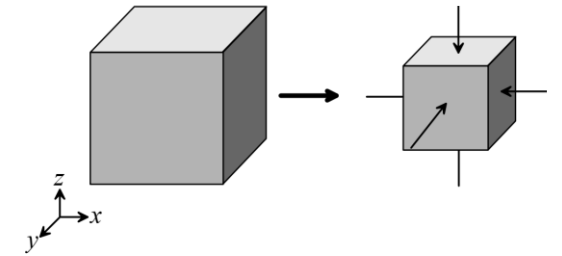


$$d\langle \sigma \rangle_{zz} = E_{oedo} \times d\langle \epsilon \rangle_{zz}$$

$$\nu = \frac{k_0}{1 + k_0} = \frac{dP_{lat}}{dP_{load} + dP_{lat}}$$

$$E = E_{oedo} \frac{(1 + \nu)(1 - 2\nu)}{1 - \nu}$$

## Transport

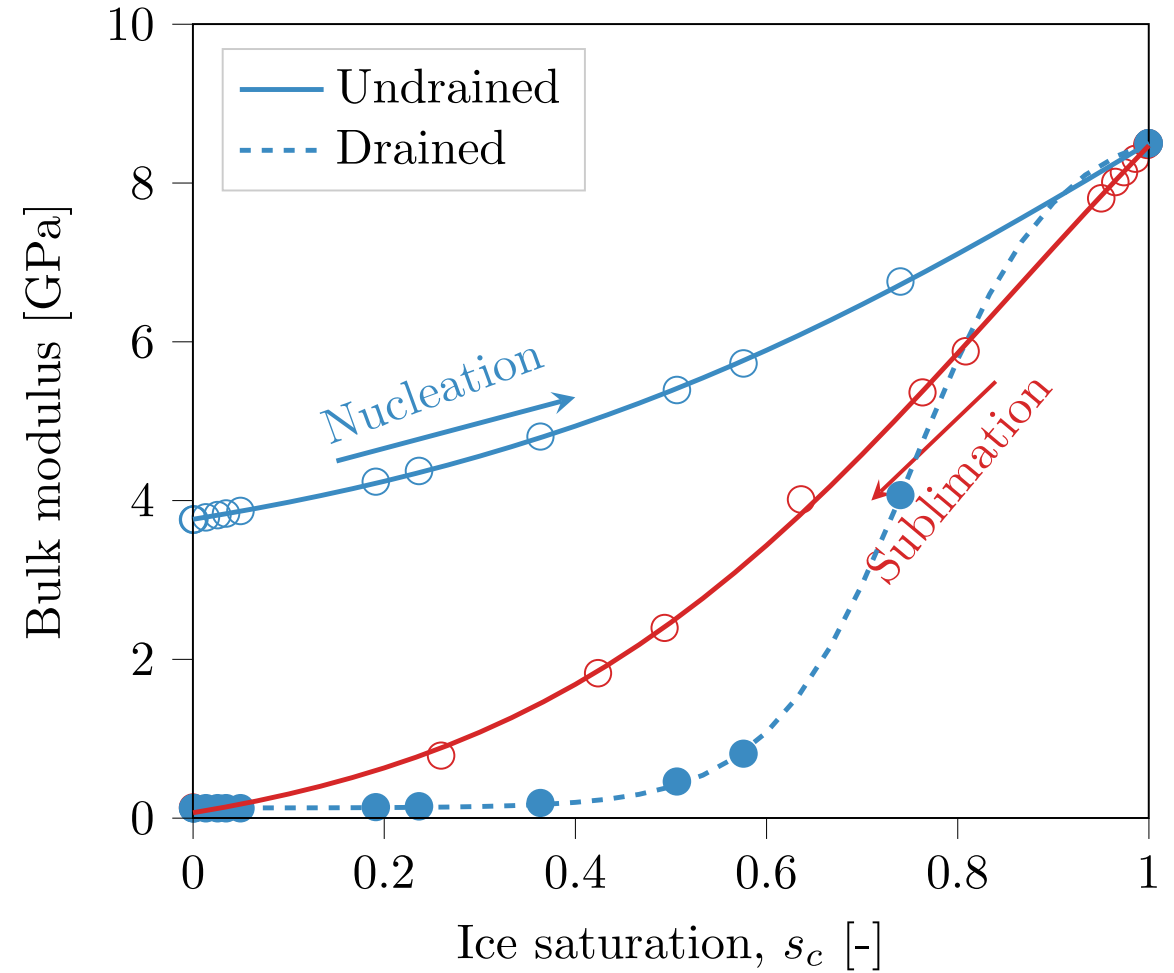
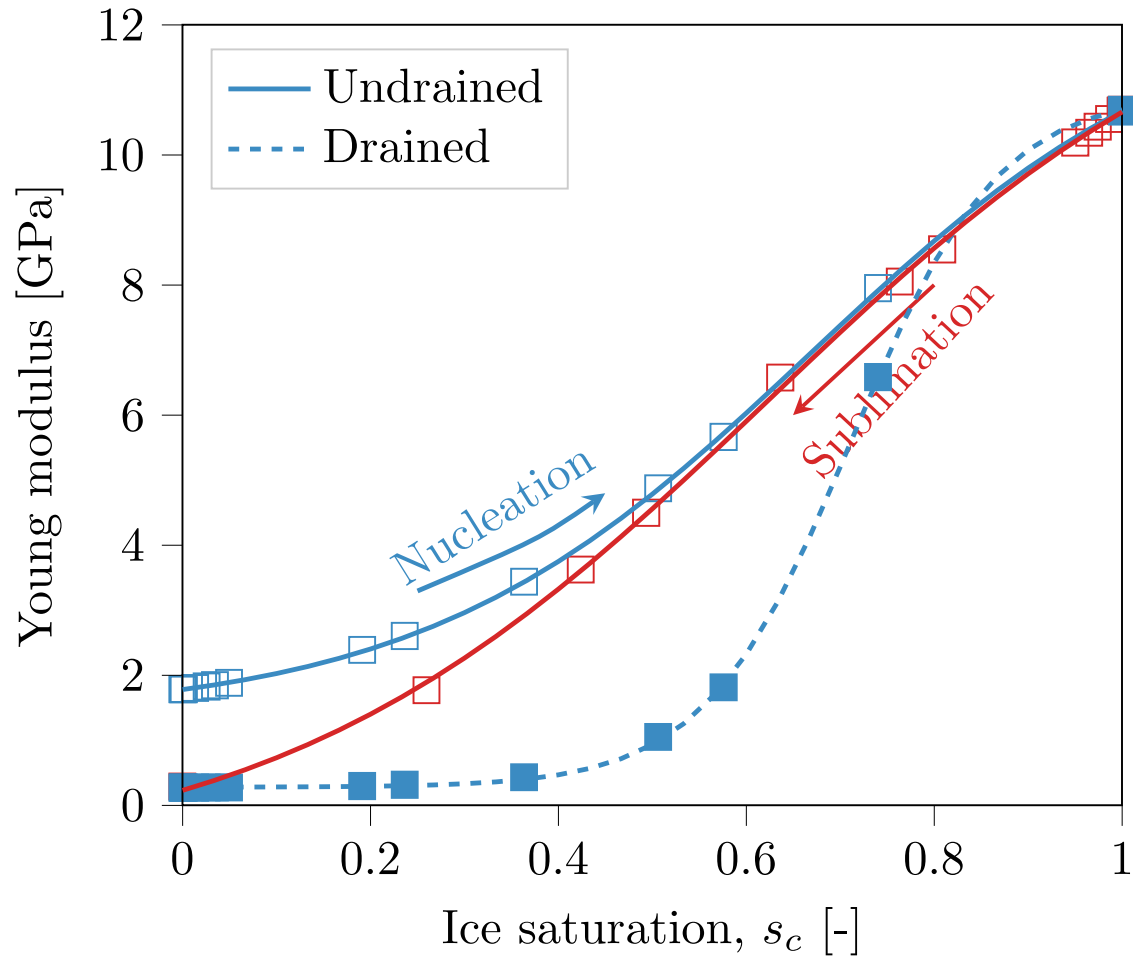


$$\langle \mathbf{q} \rangle = -\lambda^{hom} \cdot \langle \nabla(\theta) \rangle$$

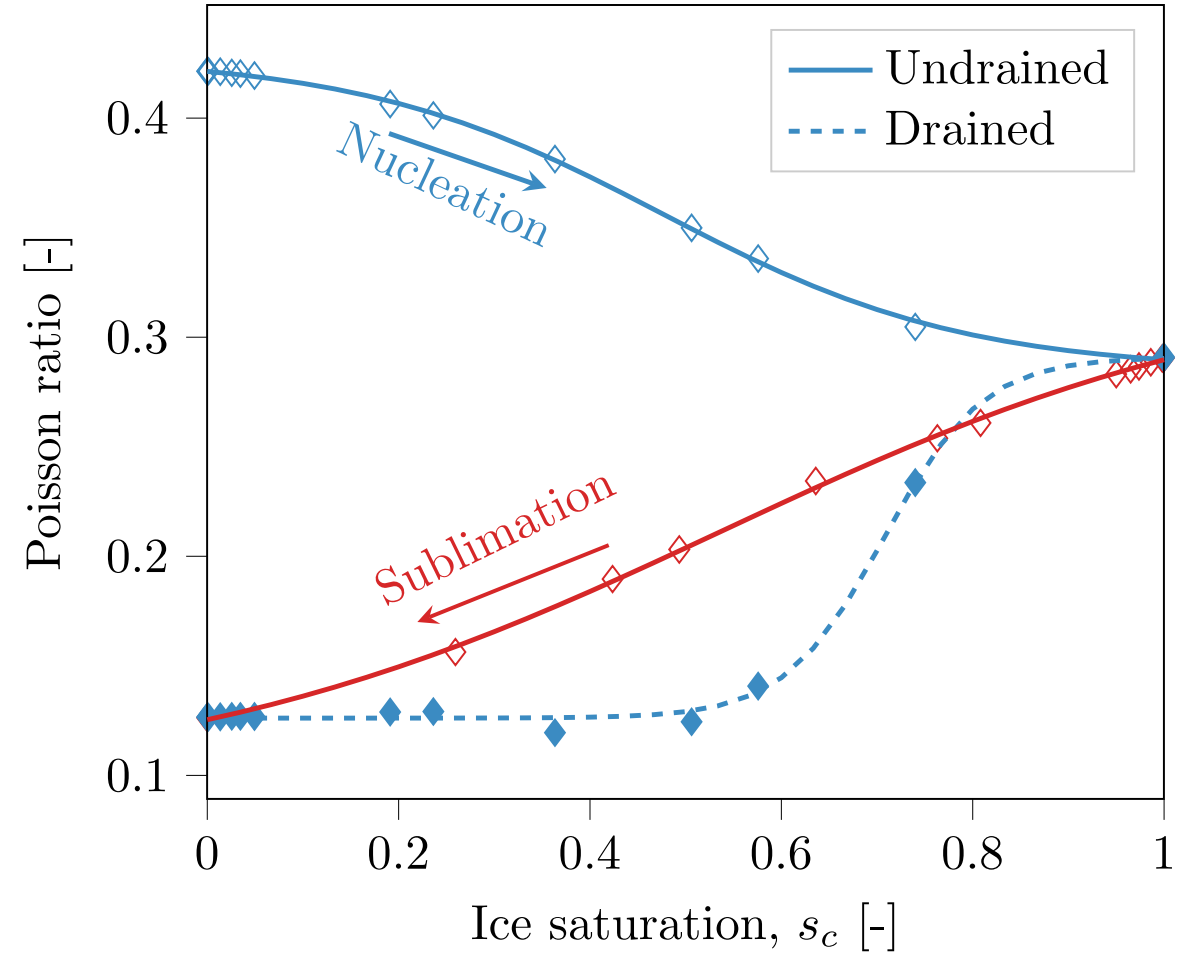
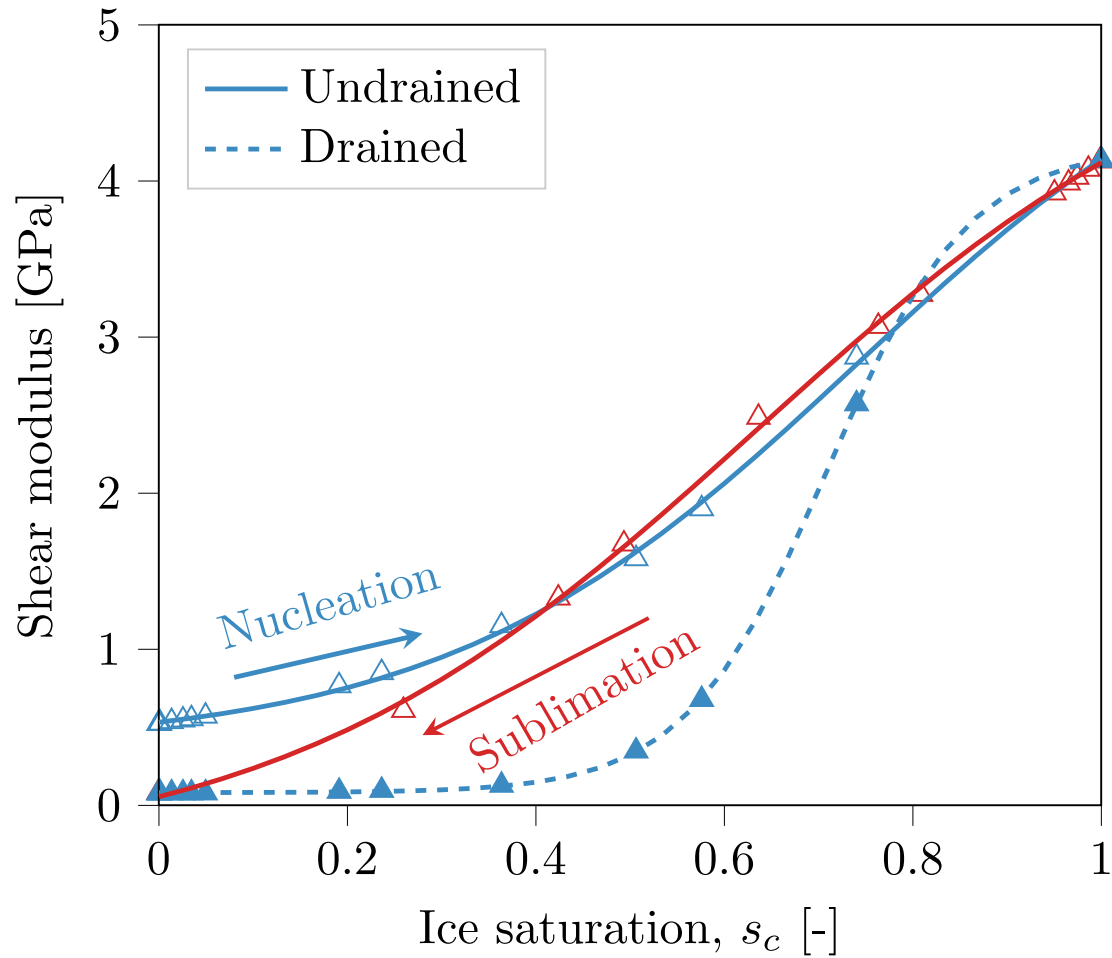
$$\langle \mathbf{w} \rangle = -\frac{\rho}{\eta} \mathbf{k}^{hom} \cdot \langle \nabla(p) \rangle$$

$$\langle \mathbf{j} \rangle = -\mathbf{d}^{hom} \cdot \langle \nabla(c) \rangle$$

# Elastic moduli as a function of water saturation

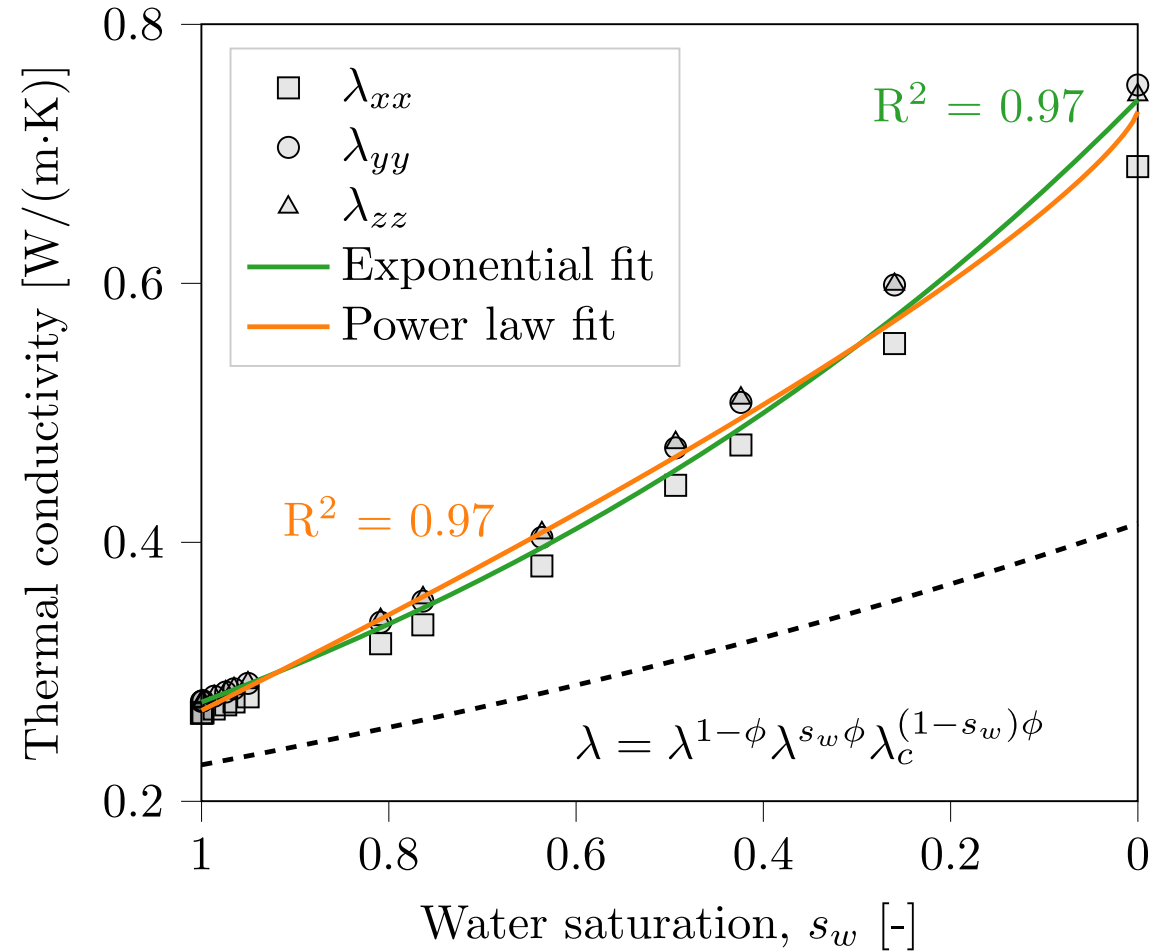
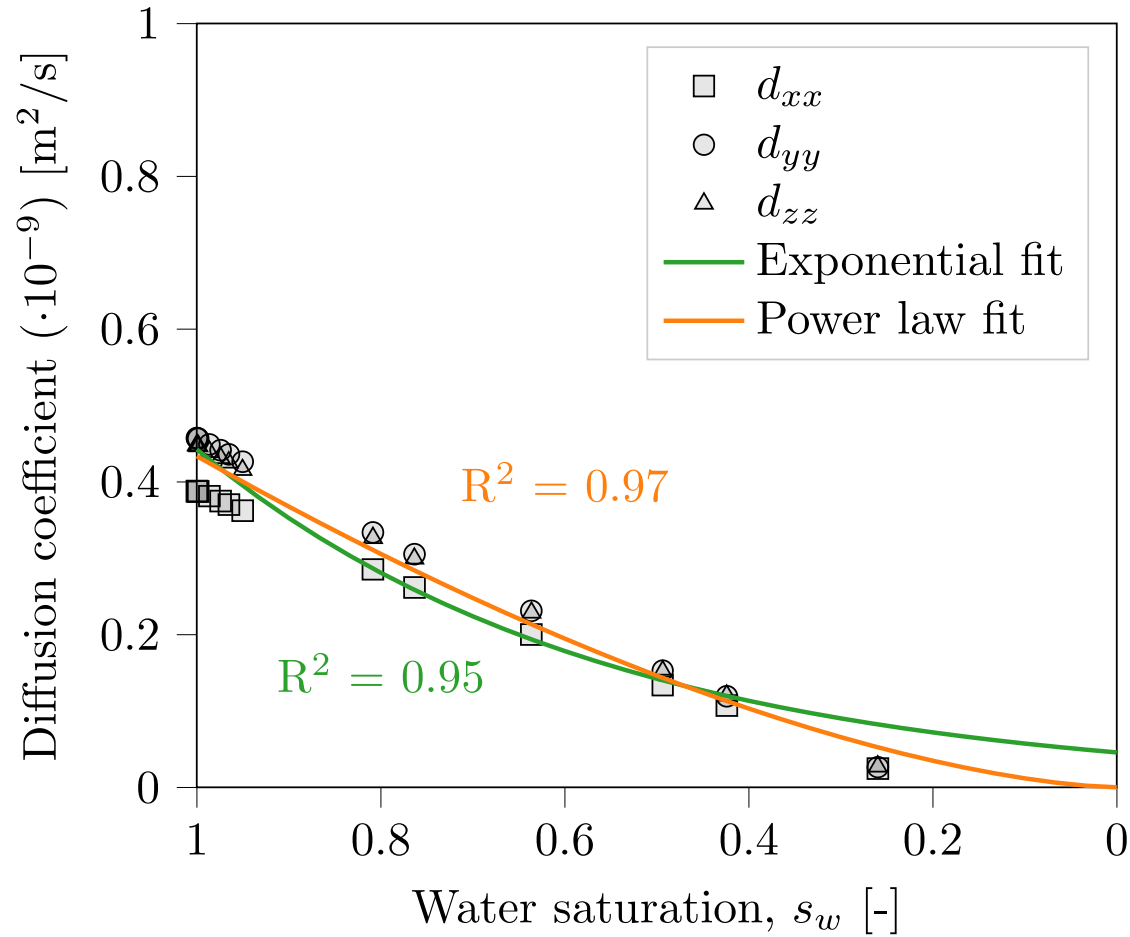


# Elastic moduli as a function of water saturation



# Transport properties during ice nucleation

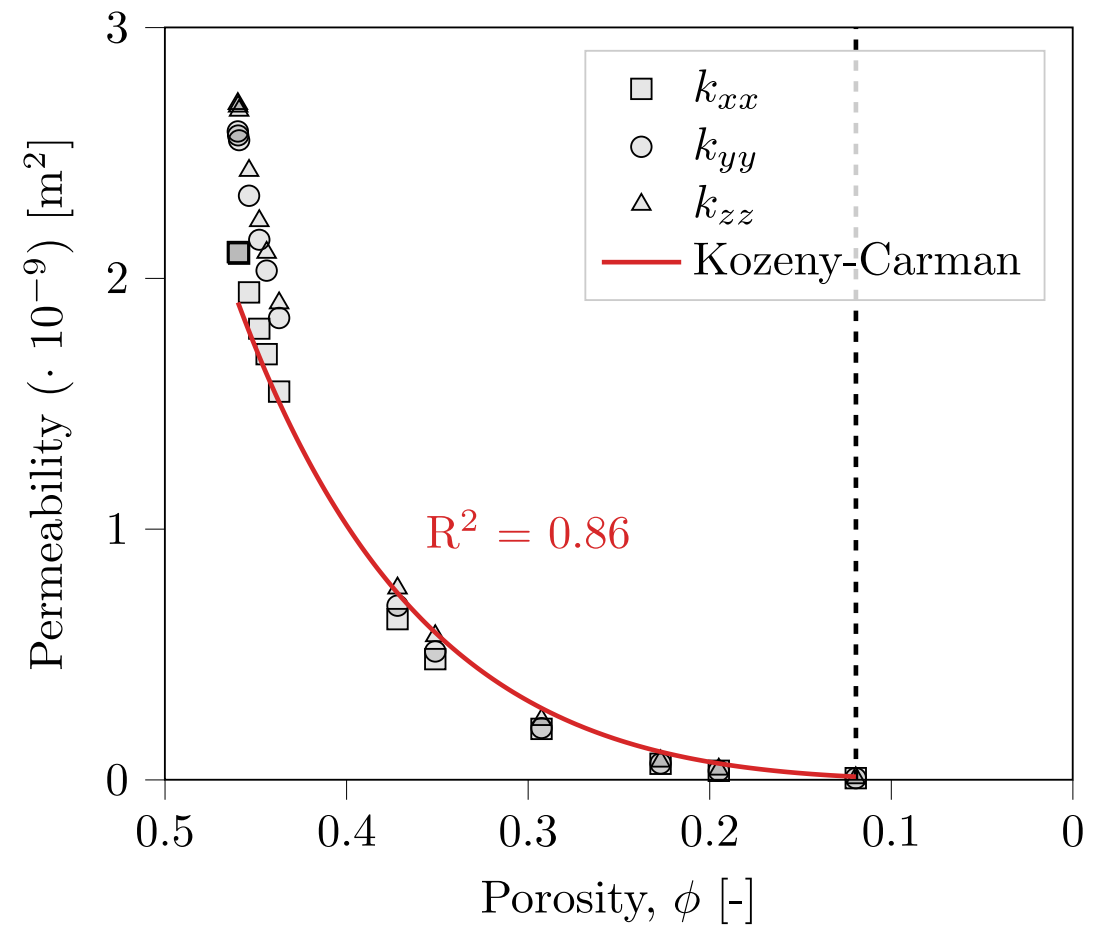
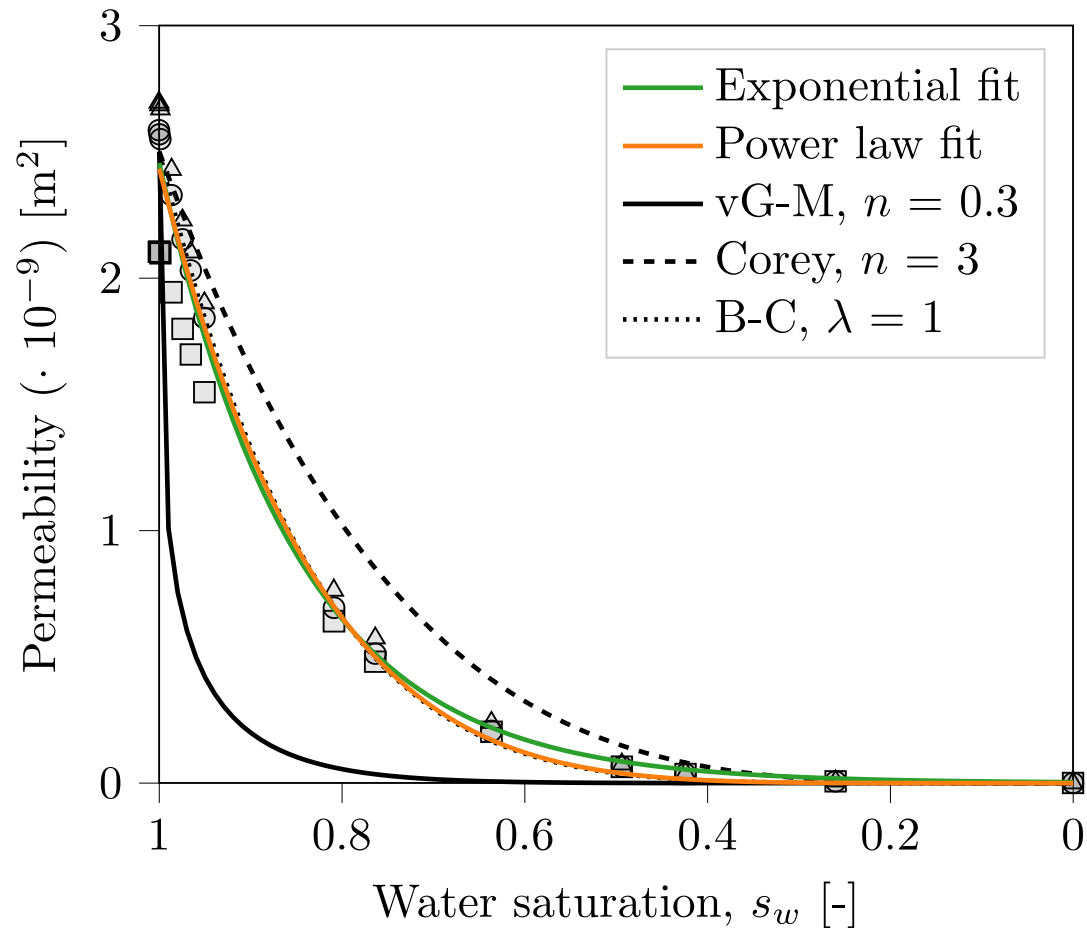
## Nucleation



# Nucleation

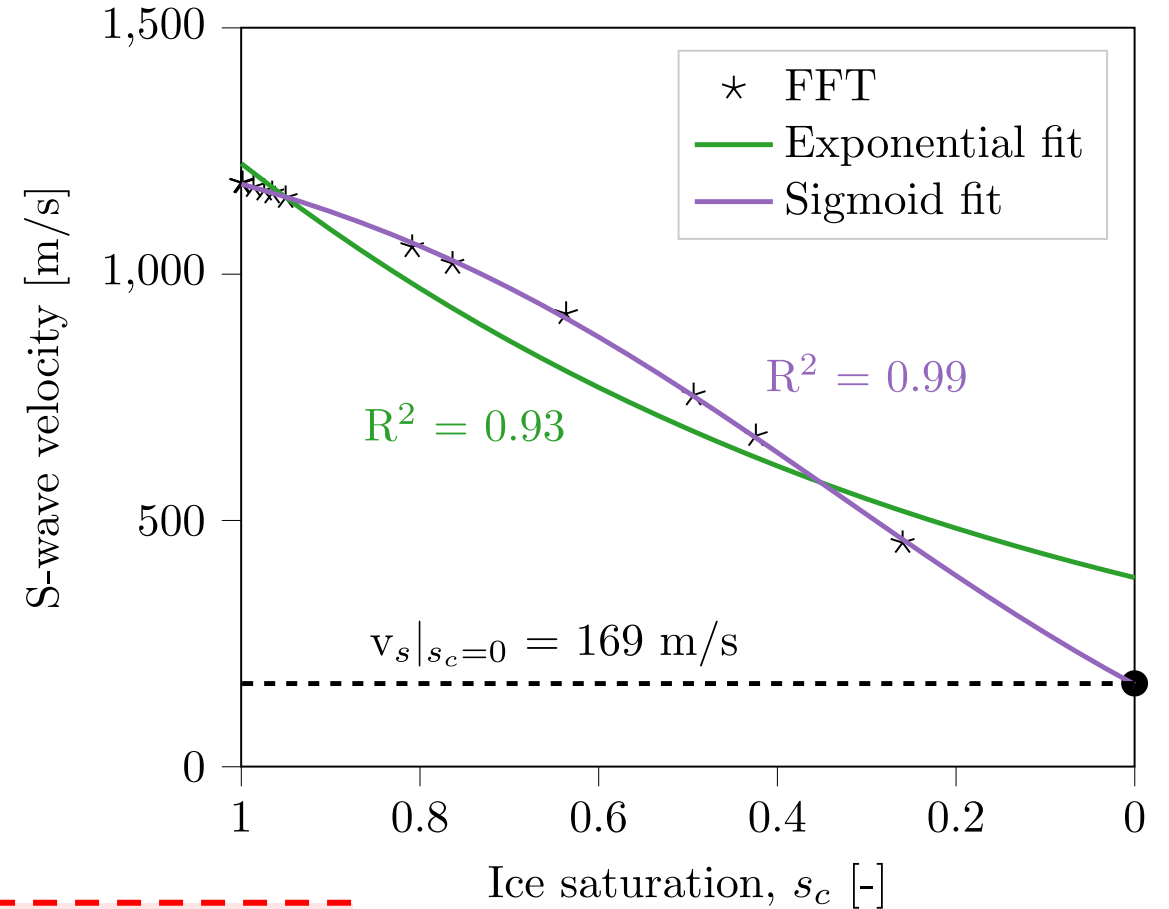
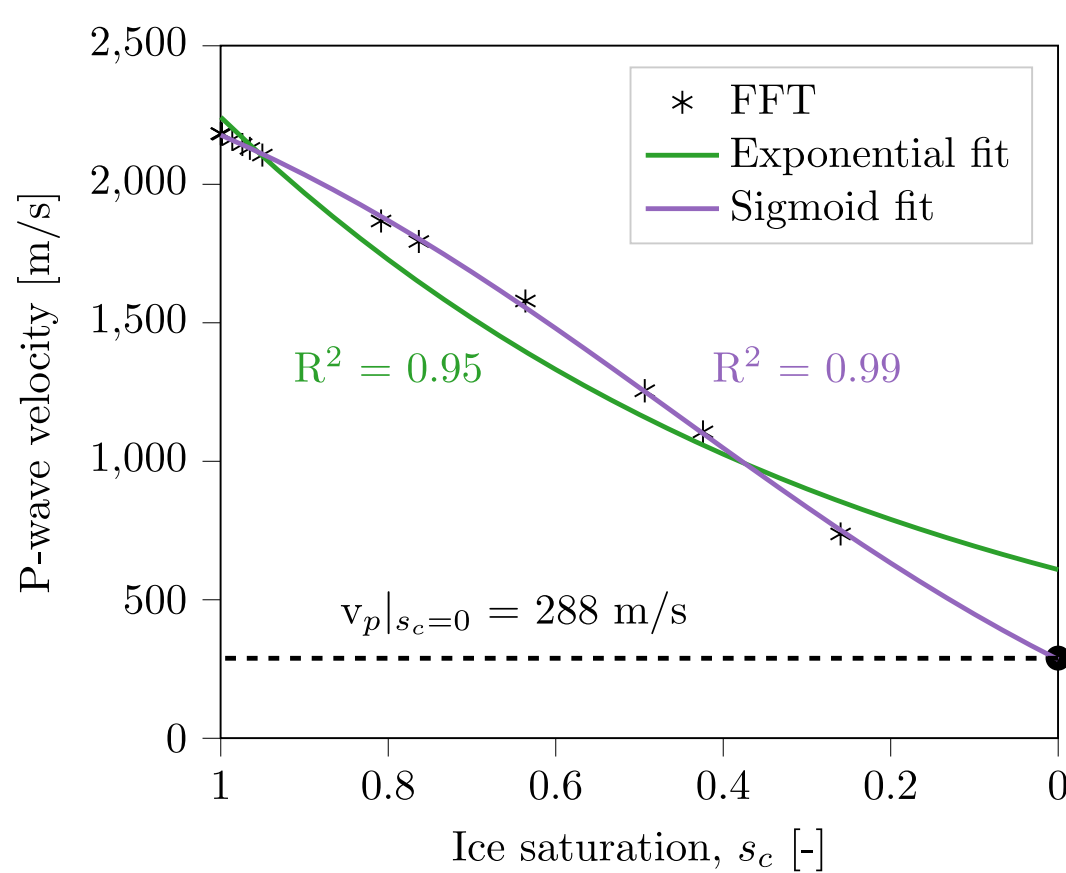
Summary of the permeability models used as comparison.

Model	Equation	Abbreviation	Reference
Brooks-Corey	$k(s_w) = k_{sat} s_w^{\frac{2+3\lambda}{\lambda}}$	B-C	[128]
van Genuchten-Mualem	$k(s_w) = k_{sat} \sqrt{s_w} \left[ 1 - \left( 1 - s_w^{1/n} \right)^n \right]^2$	vG-M	[129, 130]
Corey type	$k(s_w) = k_{sat} s_w^n$	Corey	[131]



# Relationship between seismic velocities and the mass fraction of ice

## Sublimation

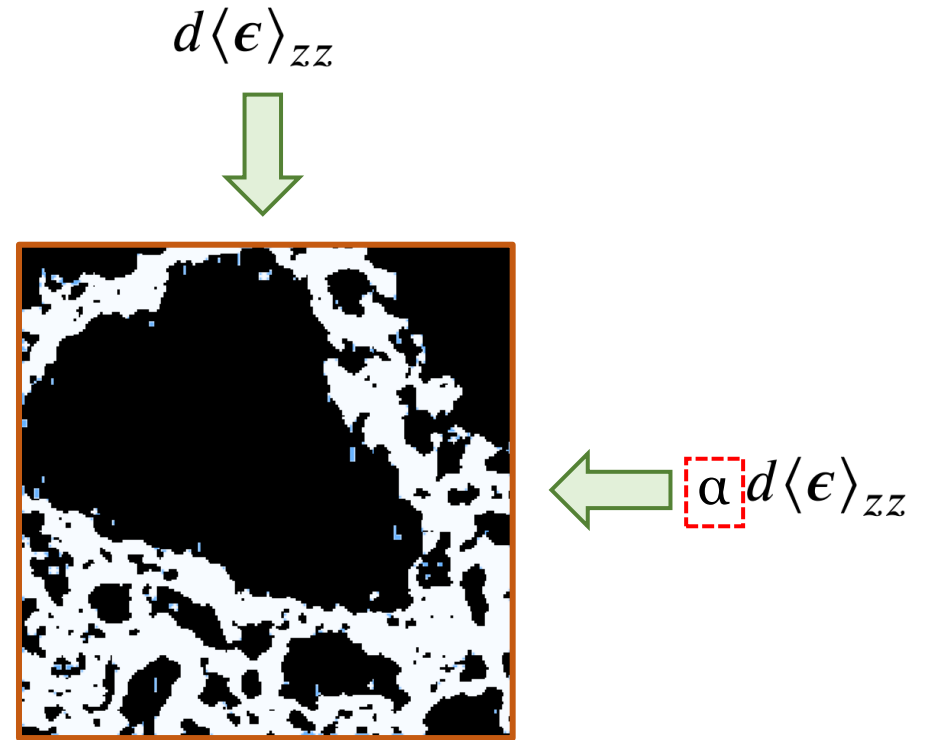
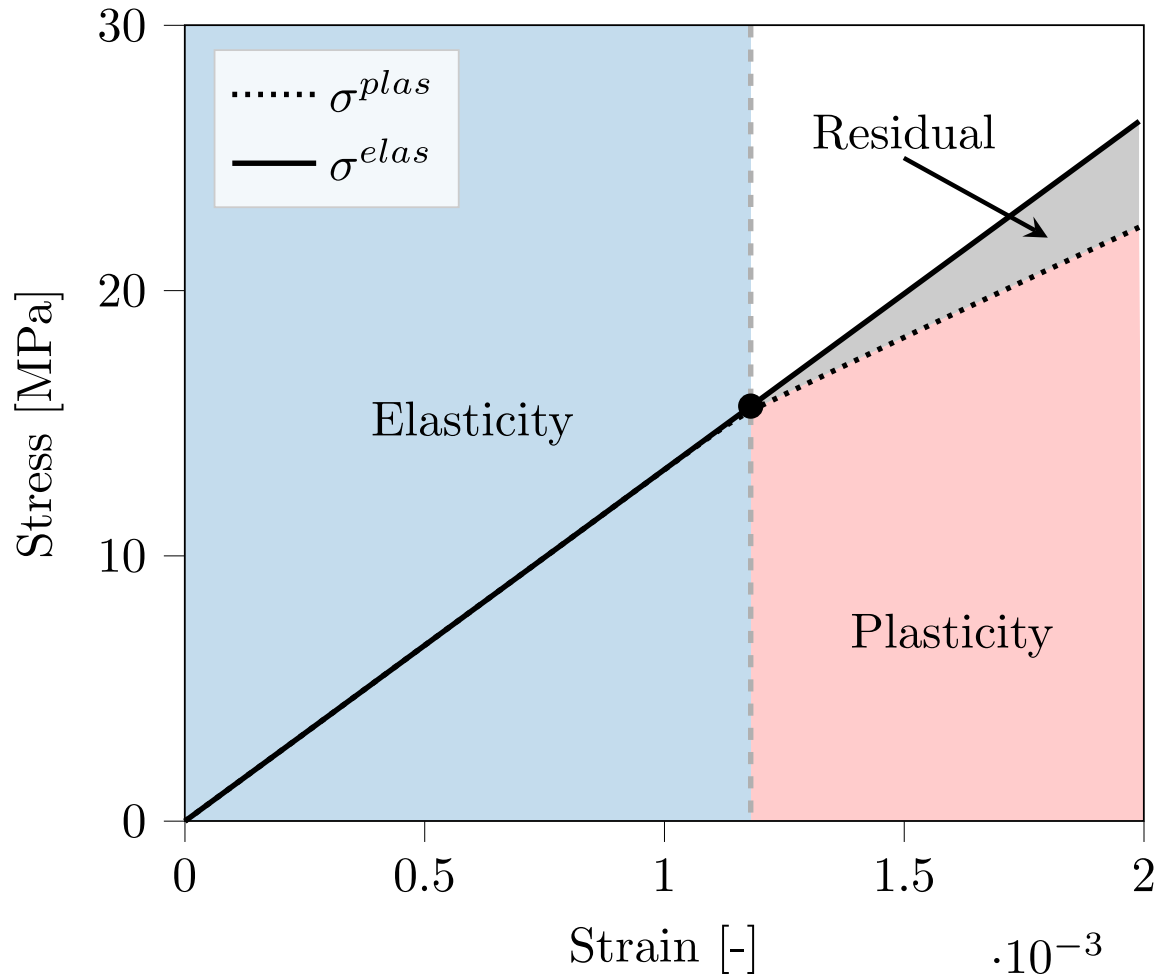


**Experimental results:**

$$v_p = 170 \text{ m/s}, v_s = 110 \text{ m/s}$$

# PLASTICITY

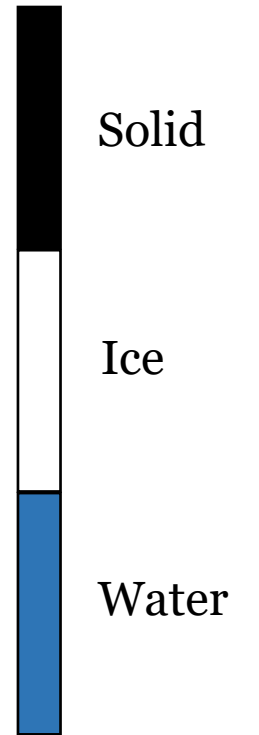
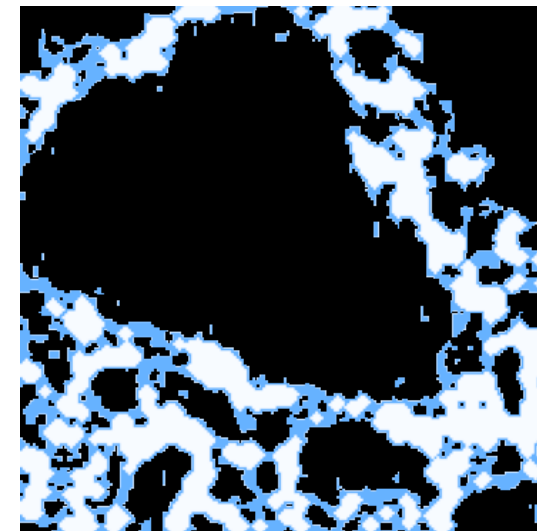
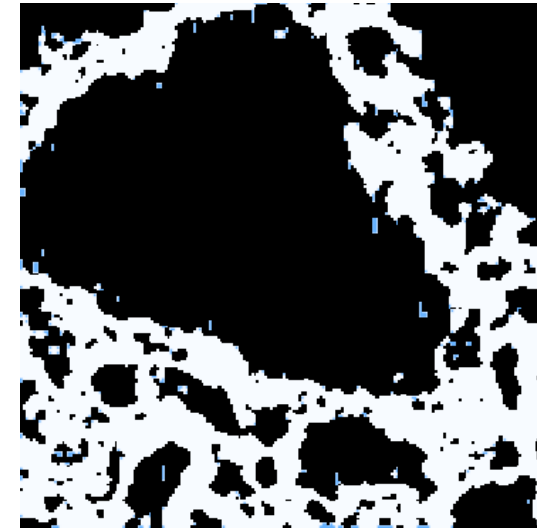
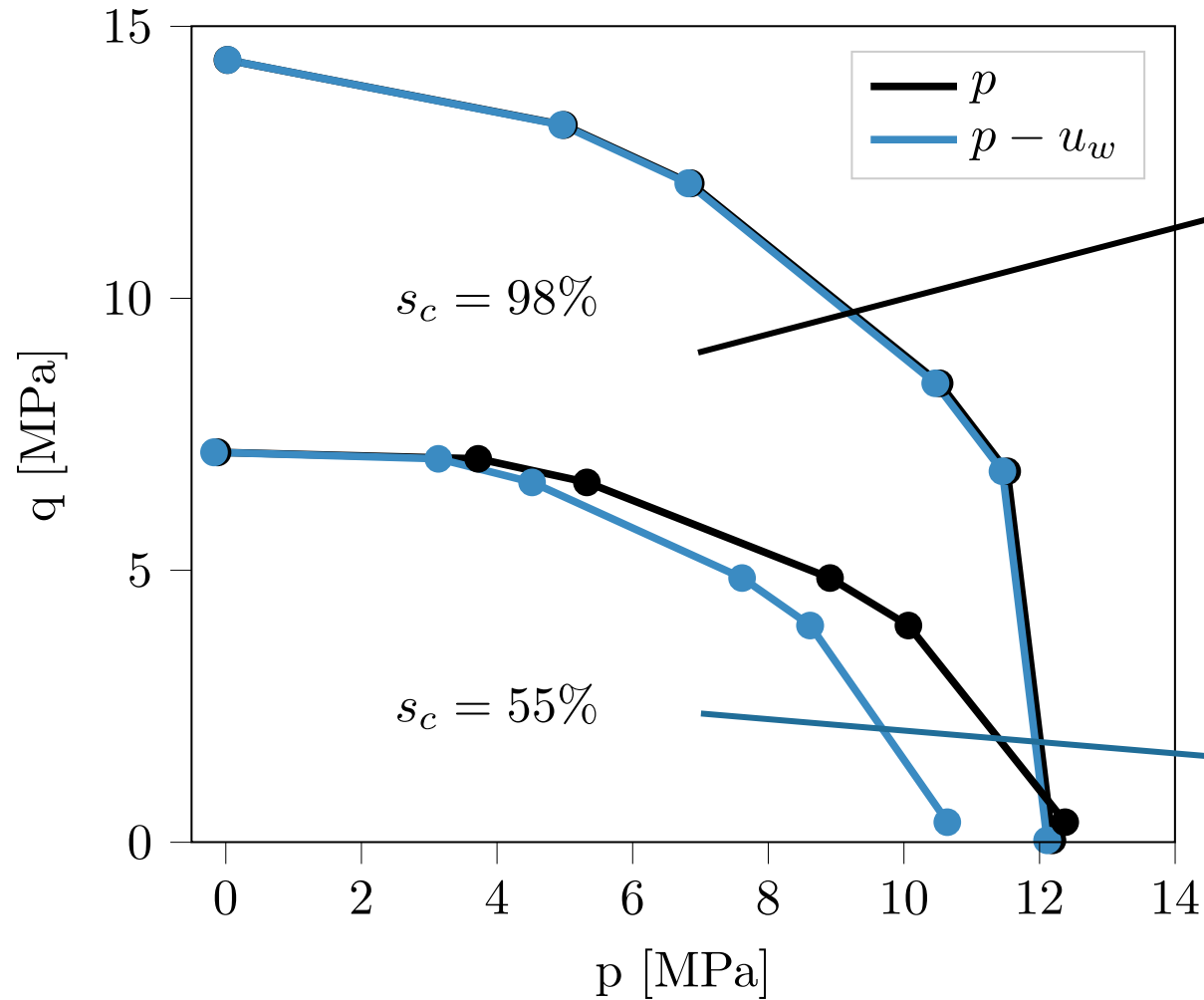
## 2D Plane strain



	$E$ [GPa]	$\nu$ [.]	yield strength (von Mises' criterion) [MPa]
Regolith	7.97	0.24	-
Water	2.2	0.48	-
Ice	9.2	0.33	13.34

Parameters of the three-phase microstructure used for the elastoplastic homogenization in frozen lunar soils.

# Yield surface as a function of ice content



## Conclusions

1. The proposed FFT-based approach accounts for thermo-hydro-elastoplastic behavior, enabling the computation of the **homogenized operators of the full THM constitutive matrix**.
2. The method remains well-defined even in the limiting cases **of infinitely soft or infinitely stiff materials**.
3. The framework is implemented and validated **for two- and three-dimensional** representative volume elements, ensuring applicability to a wide range of microstructural analyses.

Thank you