Numerical modelling of fluid-induced fault slip reactivation, application to Geo-Energy systems



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Enhangced Geothermal System (EGS) (P. Olasolo et al. , 2015)



Wastewater disposal (Manoochehr Shirzaei/ASU, 2018)



Seismicity in the geothermal site to the north of Strasbourg from March 2018 to January 2021. (Schmittbuhl et al., 2021)





Seismicity in the region surrounding the 2011 (M5.7) and 2016 (M5.8) earthquakes in Oklahoma. Epicenters of major events of the 2017 Pohang earthquake (Han-Saem Kim et al., 2018)

Aftershock4

Aftershock3

Aftershock2

Mainshock

Magnitude (M)

★ 3-4 ★ 4-5 ★ 5-6

Aftershock1

Aftershock5

Aftershock6



Drilling rig on site in St. Gallen, Switzerland (source: Webcam Project website, Aug. 7, 2013)





Horizontal meter scale map of the geological and experimental set-up (Derode et al., 2013)

mechanical weakening of the fractures (near field) \rightarrow normal stress release (across fluid-injection fracture) \rightarrow fracture slip and permeability increase



Evolution of fault frictional stability during fluid injection (Cappa et al., 2019)

Increase in fluid pressure first induces accelerating aseismic creep and fault opening. As the fluid pressure increases further, friction becomes mainly rate strengthening, favoring aseismic slip. Their study reveals how coupling between fault slip and fluid flow promotes stable fault creep during fluid injection. Seismicity is most probably triggered indirectly by the fluid injection due loading of to nonpressurized fault patches by aseismic creep





Injected fluid volume vs. maximum observed magnitude of fluid injections at different scales (Linus Villiger et al., 2020)





- > 3D finite element model
- Fault reactivation induced by fluid injection
- > Parameter study (injection rate, diffusivity, frictional parameters...)
- > How is the fault reactivated?
- > What parameters control the behavior of fault slip?







Schematic diagram of the sample assembly. (Passelegue, 2018)

Numerical model





- 3D Finite Element Model, pre-existing fault
 - Loading and boundary condition $\sigma_1 \ 0 \rightarrow 278MPa \rightarrow 90\%$ $\sigma_3 \ 100MPa$ Fluid injection: $10 \rightarrow 90MPa$ 1,10,100,1000MPa/minBottom U₂=0 Middle point fixed
- Interaction type: surface-to-surface contact

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Tangential Behavior: User-defined Slipweakening

Coulomb friction law, μ_s =0.578, μ_d =0.5. Pressure-Overclosure: "Hard" Contact Methodology



Mohr Diagram





Slip-weakening friction law

Fluid diffusion





 $\frac{\partial p}{\partial t} = D \cdot \nabla^2 p$





Numerical calibration with different young's modulus



• 5×10⁻⁶ m²/s



- Location mechanical performance difference
- Maximum slip with injection rate





Time history of shear stress and relative fault slip evolution along the fault. The solid is shear stress and the dashed is fault slip. Left: injection rate V_{ini} = 10MPa/min. Right: V_{inj} = 100MPa/min.





Fault slip tests with three groups of diffusivities and diverse injection rates.

Maximum slip dependent on fluid volume.





Parameter study of slip weakening friction law. Relationship between fault slip with dynamic friction coefficient μ_d and slip weakening threshold Dc.





Shear front along the strike and calculation of crack propagation speed





Crack propagation tests with three groups of diffusivities and diverse injection rates.



- Conclusion
- 1. Fault slip is dependent on injection rate, diffusivity and injection volume. An increase of diffusivity and injection volume results in higher fault slip. Lower injection rates lead to larger amount of fluid injected

and higher fault slip.

- 2. Crack propagation speed ranges from 1 to 300 m/day and increase with diffusivity and injection rate.
- Prospect

How initial stress and confining pressure affect fault reactivation behavior?